

ICC-ES Evaluation Report

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DIVISION: 03 00 00 — CONCRETE

Section: 03 16 00 — Concrete Anchors

DIVISION: 05 00 00 —

METALS

Section: 05 05 19 — Post-Installed Concrete

Anchors

REPORT HOLDER: ADOLF WÜRTH GmbH &

CO. KG

EVALUATION SUBJECT: WÜRTH WIT-UH 300 ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR SYSTEM IN CRACKED AND UNCRACKED CONCRETE



1.0 EVALUATION SCOPE

Compliance with the following codes:

- 2018, 2015, 2012 and 2009 *International Building Code*® (IBC)
- 2018, 2015, 2012 and 2009 International Residential Code® (IRC)

Property evaluated:

Structural

2.0 USES

The Würth WIT-UH 300 Adhesive Anchor System is used as anchorage and the Post-Installed Reinforcing Bar System is used as reinforcing bar connection (for development length and splice length) in cracked and uncracked normalweight concrete with a specified compressive strength, f_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa) to resist static, wind or earthquake (IBC Seismic Design Categories A through F) tension and shear loads.

The anchor system complies with anchors as described in Section 1901.3 of the 2018 and 2015 IBC, Section 1909 of the 2012 IBC and is an alternative to cast-in-place and post-installed anchors described in Section 1908 of the 2012 IBC, and Sections 1911 and 1912 of the 2009 IBC. The anchor system may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the IRC.

The post-installed reinforcing bar system is an alternative to cast-in-place reinforcing bar connection governed by ACI 318 and IBC Chapter 19.

3.0 DESCRIPTION

3.1 General:

The Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System is comprised of Würth WIT-UH 300 two-component adhesive filled in cartridges, static mixing nozzles, dispensing tools, hole cleaning equipment and adhesive injection accessories, and steel anchor elements, which are continuously threaded steel rods (to form the Würth WIT-UH 300 Adhesive Anchor System) or deformed steel reinforcing bars (to form the Würth WIT-UH 300 Adhesive Anchor System or the Post-Installed Reinforcing Bar System).

The primary components of the Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System, including the Würth WIT-UH 300 adhesive cartridge, static mixing nozzle, and steel anchor

elements, are shown in <u>Figures 1</u> and <u>2</u> of this report. The manufacturer's printed installation instructions (MPII), included with each adhesive unit package, are shown in <u>Figure 6</u> of this report.

3.2 Materials:

3.2.1 Würth WIT-UH 300 Adhesive: Würth WIT-UH 300 adhesive is an injectable two-component vinylesterurethane hybrid adhesive. The two components are kept separate by means of a labelled dual-cylinder cartridge. The two components combine and react when dispensed through a static mixing nozzle, supplied by Adolf Würth GmbH & Co. KG, which is attached to the cartridge. Würth WIT-UH 300 is available in: coaxial cartridges: 5-ounce (150 mL), 9.5-ounce (280 mL) up to 11-ounce (333 mL) and 13 up to 14-ounce (380 up to 420 mL) and side-by-side cartridges: 8-ounce (235 mL), 11.5-ounce (345 mL) up to 12-ounce (360 mL) and 28-ounce (825 mL).

Each cartridge label is marked with the adhesive expiration date. The shelf life, as indicated by the expiration date, applies to an unopened cartridge stored in a dry, dark, and cool environment.

- **3.2.2 Hole Cleaning Equipment:** Hole cleaning equipment is comprised of steel wire brushes supplied by Adolf Würth GmbH & Co. KG, and air blowers which are shown in <u>Figure 6</u> of this report. The Würth dust removal system shown in <u>Figure 3</u> of this report removes dust with a HEPA dust extractor during the hole drilling operation in dry base materials.
- **3.2.3 Dispensers:** Würth WIT-UH 300 adhesive must be dispensed with manual dispensers, pneumatic dispensers, or electric powered dispensers supplied by Adolf Würth GmbH & Co. KG.

3.2.4 Steel Anchor Elements:

- **3.2.4.1 Threaded Steel Rods for use in Post-Installed Anchor Applications:** Threaded steel rods must be clean and continuously threaded (all-thread) in diameters described in <u>Tables 4</u> and <u>10</u>, and <u>Figure 6</u> of this report. Specifications for grades of threaded rod, including the mechanical properties, and corresponding nuts and washers, are included in <u>Table 2</u> of this report. Carbon steel threaded rods must be furnished with a minimum 0.0002-inch-thick (0.005 mm) zinc electroplated coating complying with ASTM B633, SC1 or a minimum 0.0021-inch-thick (0.053 mm) mechanically deposited zinc coating complying with ASTM B695, Class 55. The stainless-steel threaded rods must comply with <u>Table 2</u> of this report. Steel grades and types of material (carbon, stainless) for the washers and nuts must match the threaded rods. Threaded steel rods must be clean, straight, and free of indentations or other defects along their length. The embedded end may be flat cut or cut on the bias to a chisel point.
- **3.2.4.2 Steel Reinforcing Bars for use in Post-Installed Anchor Applications:** Steel reinforcing bars must be deformed reinforcing bars as described in <u>Table 3</u> of this report. <u>Tables 7</u> and <u>13</u> and <u>Figure 6</u> summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be clean, straight, and free of mill scale, rust, mud, oil, and other coatings (other than zinc) that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation except as set forth in ACI 318-14 Section 26.6.3.1 (b) or ACI 318-11 Section 7.3.2, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- **3.2.4.3** Steel Reinforcing Bars for Use in Post-Installed Reinforcing Bar Connections: Steel reinforcing bars used in post-installed reinforcing bar connections must be deformed reinforcing bars (rebars) as depicted in <u>Figures 4</u> and <u>5</u>. <u>Tables 16</u>, <u>17</u>, and <u>Figure 6</u> summarize reinforcing bar size ranges. The embedded portions of reinforcing bars must be clean, straight, and free of mill scale, rust, mud, oil and other coatings that may impair the bond with the adhesive. Reinforcing bars must not be bent after installation, except as set forth in Section 26.6.3.1(a) of ACI 318-14 or Section 7.3.2 of ACI 318-11, as applicable, with the additional condition that the bars must be bent cold, and heating of reinforcing bars to facilitate field bending is not permitted.
- **3.2.4.4 Ductility:** In accordance with ACI 318-14 Section 2.3 or ACI 318-11 Appendix D Section D.1, as applicable, in order for a steel anchor element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation less than 14 percent or a reduction of area less than 30 percent, or both, are considered brittle. Specifications and physical properties of various steel materials are provided for threaded rods in <u>Table 2</u> and for threaded rods in <u>Table 3</u> of this report. Where values are nonconforming or unstated, the steel must be considered brittle.

3.3 Concrete:

Normalweight concrete must comply with Sections 1903 and 1905 of the IBC. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

4.0 DESIGN AND INSTALLATION

4.1 Strength Design of Post-Installed Anchors:

4.1.1 General: The design strength of anchors under the 2018 and 2015 IBC, as well as the 2018 and 2015 IRC, must be determined in accordance with ACI 318-14 and this report. The design strength of anchors under the 2012 and 2009 IBC, as well as the 2012 and 2009 IRC, must be determined in accordance with ACI 318-11 and this report.

The strength design of anchors must comply with ACI 318-14 17.3.1 or 318-11 D.4.1, as applicable, except as required in ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable.

Design parameters are provided in Tables 4 through Table 15 of this report.

Strength reduction factors, ϕ , as given in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, must be used for load combinations calculated in accordance with Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable.

Strength reduction factors, ϕ , as given in ACI 318-11 D.4.4 must be used for load combinations calculated in accordance with ACI 318-11 Appendix C.

- **4.1.2 Static Steel Strength in Tension:** The nominal static steel strength of a single anchor in tension, N_{sa} , in accordance with ACI 318-14 17.4.1.2 or ACI 318-11 D.5.1.2, as applicable, and the associated strength reduction factors, ϕ , in accordance with ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are provided in Tables 4, 7, 10 and 13 of this report for the corresponding anchor steel.
- **4.1.3 Static Concrete Breakout Strength in Tension:** The nominal static concrete breakout strength of a single anchor or group of anchors in tension, N_{cb} or N_{cbg} , must be calculated in accordance with ACI 318-14 17.4.2 or ACI 318-11 D.5.2, as applicable, with the following addition:

The basic concrete breakout strength of a single anchor in tension, N_b , must be calculated in accordance with ACI 318-14 17.4.2.2 or ACI 318-11 D.5.2.2, as applicable, using the values of $k_{c,cr}$ and $k_{c,uncr}$ as provided in Tables 5, 8, 11 and 14 of this report. Where analysis indicates no cracking in accordance with ACI 318-14 17.4.2.6 or ACI 318-11 D.5.2.6, as applicable, N_b must be calculated using $k_{c,uncr}$ and $\Psi_{c,N}$ = 1.0. For anchors in lightweight concrete see ACI 318-14 17.2.6 or ACI 318-11 D.3.6, as applicable. The value of f_c used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable. The value of f_c used for calculation must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars in cracked concrete. Additional information for the determination of nominal bond strength in tension is given in Section 4.1.4 of this report.

4.1.4 Static Bond Strength in Tension: The nominal static bond strength of a single adhesive anchor or group of adhesive anchors in tension, N_a or N_{ag} , must be calculated in accordance with ACI 318-14 17.4.5 or ACI 318-11 D.5.5, as applicable.

Bond strength values ($\tau_{k,cr}$, $\tau_{k,uncr}$) are a function of concrete compressive strength, concrete state (cracked, uncracked) and installation conditions (dry concrete, water-saturated concrete, water-filled holes). Special inspection level is qualified as periodic for all anchors except as shown in Section 4.3 of this report (the selection of continuous special inspection level does not provide an increase in anchor category or associated strength reduction factor for design). The following table summarizes the requirements:

CONCRETE STATE	BOND STRENGTH	CONCRETE COMPRESSIVE STRENGTH	PERMISSIBLE INSTALLATION CONDITIONS	ASSOCIATED STRENGTH REDUCTION FACTOR
			Dry concrete	ϕ a
cracked	Tk,cr		Water-saturated concrete	ϕ ws
		f'c	Water-filled holes	$\phi_{ m wf}$
			Dry concrete	фа
uncracked	Tk,uncr		Water-saturated concrete	$\phi_{\sf WS}$
			Water- filled holes	ϕ_{W}

Strength reduction factors for determination of the bond strength are given in <u>Tables 6</u>, <u>9</u>, <u>12</u> and <u>15</u> of this report. Adjustments to the bond strength may also be made for increased concrete compressive strength as noted in the footnotes to the corresponding tables and this section.

The bond strength values in <u>Tables 6</u>, <u>9</u>, <u>12</u> and <u>15</u> of this report correspond to concrete compressive strength f_c equal to 2,500 psi (17.2 MPa). For concrete compressive strength, f_c , between 2,500 psi and 8,000 psi (17.2 MPa and 55 MPa), the tabulated characteristic bond strength may be increased by a factor of $(f_c/2,500)^{0.10}$ [For **SI**: $(f_c/17.2)^{0.10}$]. The value of f_c used for calculation must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars in cracked concrete. Where applicable, the modified bond strength values must be used in lieu of $\tau_{k,cr}$ and $\tau_{k,uncr}$ in ACI 318-14 Equations (17.4.5.1d) and (17.4.5.2) or ACI 318-11 Equations (D-21) and (D-22), as applicable.

The resulting nominal bond strength must be multiplied by the associated strength reduction factor ϕ_d , ϕ_{ws} or ϕ_{wf} , as applicable.

- **4.1.5 Static Steel Strength in Shear:** The nominal static steel strength of a single anchor in shear as governed by the steel, V_{sa} , in accordance with ACI 318-14 17.5.1.2 or ACI 318-11 D.6.1.2, as applicable, and the strength reduction factor, ϕ , in accordance with ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are given in Tables 4, 7, 11 and 13 of this report for the corresponding anchor steel.
- **4.1.6 Static Concrete Breakout Strength in Shear:** The nominal static concrete breakout strength of a single anchor or group of anchors in shear, V_{cb} or V_{cbg} , must be calculated in accordance with ACI 318-14 17.5.2 or 318-11 D.6.2, as applicable, based on information given in <u>Tables 5</u>, 8, 12 and 14 in this report.

The basic concrete breakout strength of a single anchor in shear, V_b , must be calculated in accordance with ACI 318-14 17.5.2.2 or ACI 318-11 D.6.2.2, as applicable, using the values of d given in Tables 5, 8, 12 and 14 of this report for the corresponding anchor steel in lieu of d_e . In addition, h_{ef} must be substituted for ℓ_e . In no case shall ℓ_e exceed 8d. The value of f_c shall be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318-14 17.2.7 or ACI 318-11 D.3.7, as applicable.

- **4.1.7 Static Concrete Pryout Strength in Shear:** The nominal static pryout strength of a single anchor or group of anchors in shear, V_{cp} or V_{cpg} , shall be calculated in accordance with ACI 318-14 17.5.3 or ACI 318-11 D.6.3, as applicable.
- **4.1.8 Interaction of Tensile and Shear Forces:** For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-14 17.6 or ACI 318-11 D.7, as applicable.
- **4.1.9 Minimum Member Thickness** h_{min} , **Anchor Spacing** s_{min} , **Edge Distance** c_{min} : In lieu of ACI 318-14 17.7.1 and 17.7.3 or ACI 318-11 D.8.1 and D.8.3, as applicable, values of s_{min} and c_{min} described in this report must be observed for anchor design and installation. The minimum member thicknesses, h_{min} , described in this report must be observed for anchor design and installation. For adhesive anchors that will remain untorqued, ACI 318-14 17.7.4 or ACI 318-11 D.8.4 applies, as applicable.

For anchors that will be torqued during installation, the maximum torque, T_{max} , must be reduced for edge distances less than the values given in <u>Tables 5</u>, <u>8</u>, <u>11</u> and <u>14</u> as applicable. T_{max} is subject to the edge distance, c_{min} , and anchor spacing, s_{min} , and shall comply with the following requirements:

INSTALLATION TORQUE SUBJECT TO EDGE DISTANCE										
NOMINAL ANCHOR SIZE, d	MINIMUM EDGE DISTANCE, c _{min}	MINIMUM ANCHOR SPACING, s _{min}	MAXIMUM TORQUE, T _{max}							
⁵ / ₈ in. to 1 in. #5 to #8 M16 to M24 ø14 to ø25	1.75 in. (44.5 mm)	5 <i>d</i>	0.45· T _{max}							
1 ¹ / ₄ in. #9 to #10 M27 to M30 ø28 to ø32	2.75 in. (70 mm)									

For values of T_{max} , see Figure 6 of this report.

4.1.10 Critical Edge Distance c_{ac} and $\psi_{cp,Na}$: The modification factor $\psi_{cp,Na}$, must be determined in accordance with ACI 318-14 17.4.5.5 or ACI 318-11 D.5.5.5, as applicable, except as noted below:

For all cases where c_{Na}/c_{ac} <1.0, $\psi_{cp,Na}$ determined from ACI 318-14 Eq. 17.4.5.5b or ACI 318-11 Eq. D-27, as applicable, need not be taken less than c_{Na}/c_{ac} . For all other cases, $\psi_{cp,Na}$ shall be taken as 1.0.

The critical edge distance, c_{ac} must be calculated according to Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11, in lieu of ACI 318-14 17.7.6 or ACI 318-11 D.8.6, as applicable.

$$c_{ac} = h_{ef} \cdot \left(\frac{\tau_{k, uncr}}{1160}\right)^{0.4} \cdot \left[3.1 - 0.7 \frac{h}{h_{ef}}\right]$$

(Eq. 17.4.5.5c for ACI 318-14 or Eq. D-27a for ACI 318-11)

where

 $\left[\frac{h}{h_{\rm nf}}\right]$ need not be taken as larger than 2.4; and

 $\tau_{k,uncr}$ = the characteristic bond strength stated in the tables of this report whereby $\tau_{k,uncr}$ need not be taken as larger than:

 τk , $uncr = kuncrheffc'\pi \cdot da$ Eq. (4-1)

4.1.11 Requirements for Seismic Design Categories C, D, E and F: In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchors must be designed in accordance with ACI 318-14 17.2.3 or ACI 318-11 D.3.3, as applicable, except as described below.

The nominal steel shear strength, V_{sa} , must be adjusted by $\alpha_{V,seis}$ as given in <u>Tables 4</u>, <u>7</u>, <u>11</u> and <u>13</u> for the corresponding anchor steel. The nominal bond strength $\tau_{\kappa,cr}$ must be adjusted by $\alpha_{N,seis}$ as given in <u>Tables 6</u> and <u>12</u> for threaded rods, and <u>Tables 9</u> and <u>15</u> for reinforcing bars.

As an exception to ACI 318-11 Section D.3.3.4.2: Anchors designed to resist wall out-of-plane forces with design strengths equal to or greater than the force determined in accordance with ASCE 7 Equation 12.11-1 or 12.14-10 shall be deemed to satisfy ACI 318-11 Section D.3.3.4.3(d).

Under ACI 318-11 D.3.3.4.3(d), in lieu of requiring the anchor design tensile strength to satisfy the tensile strength requirements of ACI 318-11 D.4.1.1, the anchor design tensile strength shall be calculated from ACI 318-11 D.3.3.4.4.

The following exceptions apply to ACI 318-11 D.3.3.5.2:

- 1. For the calculation of the in-plane shear strength of anchor bolts attaching wood sill plates of bearing or non-bearing walls of light-frame wood structures to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
- 1.1. The allowable in-plane shear strength of the anchor is determined in accordance with AF&PA NDS Table 11E for lateral design values parallel to grain.
- 1.2. The maximum anchor nominal diameter is ⁵/₈ inch (16 mm).
- 1.3. Anchor bolts are embedded into concrete a minimum of 7 inches (178 mm).
- 1.4. Anchor bolts are located a minimum of $1^{3}/_{4}$ inches (45 mm) from the edge of the concrete parallel to the length of the wood sill plate.
- 1.5. Anchor bolts are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the wood sill plate.
- 1.6. The sill plate is 2-inch or 3-inch nominal thickness.
- 2. For the calculation of the in-plane shear strength of anchor bolts attaching cold-formed steel track of bearing or non-bearing walls of light-frame construction to foundations or foundation stem walls, the in-plane shear strength in accordance with ACI 318-11 D.6.2 and D.6.3 need not be computed and ACI 318-11 D.3.3.5.3 need not apply provided all of the following are satisfied:
 - 2.1. The maximum anchor nominal diameter is 5/8 inch (16 mm).
 - 2.2. Anchors are embedded into concrete a minimum of 7 inches (178 mm).
- 2.3. Anchors are located a minimum of $1^{3}/_{4}$ inches (45 mm) from the edge of the concrete parallel to the length of the track.
- 2.4. Anchors are located a minimum of 15 anchor diameters from the edge of the concrete perpendicular to the length of the track.

2.5. The track is 33 to 68 mil designation thickness.

Allowable in-plane shear strength of exempt anchors, parallel to the edge of concrete shall be permitted to be determined in accordance with AISI S100 Section E3.3.1.

3. In light-frame construction, bearing or nonbearing walls, shear strength of concrete anchors less than or equal to 1 inch [25 mm] in diameter attaching a sill plate or track to foundation or foundation stem wall need not satisfy ACI 318-11 D.3.3.5.3(a) through (c) when the design strength of the anchors is determined in accordance with ACI 318-11 D.6.2.1(c).

4.2 Strength Design of Post-Installed Reinforcing Bars:

4.2.1 General: The design of straight post-installed deformed reinforcing bars must be determined in accordance with ACI 318 rules for cast-in place reinforcing bar development and splices and this report.

Examples of typical applications for the use of post-installed reinforcing bars are illustrated in <u>Figure 5</u> of this report.

4.2.2 Determination of bar development length I_d : Values of I_d must be determined in accordance with the ACI 318 development and splice length requirements for straight cast-in place reinforcing bars.

Exceptions:

- 1. For uncoated and zinc-coated (galvanized) post-installed reinforcing bars, the factor Ψ_e shall be taken as 1.0. For all other cases, the requirements in ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (b) shall apply.
- 2. When using alternate methods to calculate the development length (e.g., anchor theory), the applicable factors for post-installed anchors generally apply.
- **4.2.3 Minimum Member Thickness,** h_{min} , **Minimum Concrete Cover,** $c_{c,min}$, **Minimum Concrete Edge Distance,** $c_{b,min}$, **Minimum Spacing,** $s_{b,min}$: For post-installed reinforcing bars, there is no limit on the minimum member thickness. In general, all requirements on concrete cover and spacing applicable to straight cast-in bars designed in accordance with ACI 318 shall be maintained.

For post-installed reinforcing bars installed at embedment depths, h_{ef} , larger than 20d ($h_{ef} > 20d$), the minimum concrete cover shall be as follows:

REBAR SIZE	MINIMUM CONCRETE COVER, $c_{c,min}$
d _b ≤ No. 6 (16mm)	1 ³ / ₁₆ in. (30mm)
No. $6 < d_b \le No.10$ (16mm $< d_b \le 32mm$)	1 ⁹ / ₁₆ in. (40mm)

The following requirements apply for minimum concrete edge and spacing for $h_{ef} > 20d$:

Required minimum edge distance for post-installed reinforcing bars (measured from the center of the bar):

 $c_{b,min} = d_0/2 + c_{c,min}$

Required minimum center-to-center spacing between post-installed bars:

 $s_{b,min} = d_0 + c_{c,min}$

Required minimum center-to-center spacing from existing (parallel) reinforcing:

 $s_{b,min} = d_b/2$ (existing reinforcing) + $d_0/2$ + $c_{c,min}$

4.2.4 Design Strength in Seismic Design Categories C, D, E and F: In structures assigned to Seismic Category C, D, E or F under the IBC or IRC, design of straight post-installed reinforcing bars must take into account the provisions of ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21, as applicable.

4.3 Installation:

Installation parameters are illustrated in Figure 1 of this report. Installation must be in accordance with ACI 318-14 17.8.1 and 17.8.2 or ACI 318-11 D.9.1 and D.9.2. Anchor and post-installed reinforcing bar locations must comply with this report and the plans and specifications approved by the code official. Installation of the Würth WIT-UH 300 Adhesive Anchor and Post-Installed Reinforcing Bar Systems must conform to the manufacturer's printed installation instructions included in each unit package and provided in Figure 6 of this report.

The adhesive anchor system may be used for upwardly inclined orientation applications (e.g., overhead). Upwardly inclined and horizontal orientation applications are to be installed using piston plugs for the ⁵/₈-inch-

through 1^{1} /₄-inch-diameter (M16 through M30) threaded steel rods and No. 5 through No. 10 (14 mm through 32 mm) steel reinforcing bars, installed in the specified hole diameter, and attached to the mixing nozzle and extension tube supplied by Adolf Würth GmbH & Co. KG as described in Figure 6 in this report. Upwardly inclined and horizontal orientation installation for the 3 /₈-inch- and 1 /₂-inch-diameter (M10 and M12) threaded steel rods, and No. 3 and No. 4 (10 mm and 12 mm) steel reinforcing bars may be injected directly to the end of the hole using a mixing nozzle with a bore hole depth $d_0 \le 10$ " (250 mm).

Installation of anchors in horizontal or upwardly inclined (overhead) orientations shall be fully restrained from movement throughout the specified curing period through the use of temporary wedges, external supports, or other methods. Where temporary restraint devices are used, their use shall not result in impairment of the anchor shear resistance.

4.4 Special Inspection:

Periodic special inspection must be performed where required in accordance with Section 1705.1.1 and Table 1705.3 of the 2018, 2015 and 2012 IBC, 1704.4 and 1704.15 of the 2009 IBC and this report. The special inspector must be on the jobsite initially during anchor or post-installed reinforcing bar installation to verify the anchor or post-installed reinforcing bar type and dimensions, adhesive expiration date, concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, spacing, edge distances, concrete thickness, anchor, or post-installed reinforcing bar embedment, tightening torque, and adherence to the manufacturers printed installation instructions.

The special inspector must verify the initial installations of each type and size of adhesive anchor or post-installed reinforcing bar by construction personnel on site. Subsequent installations of the same anchor or post-installed reinforcing bar type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor or post-installed reinforcing bar product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

Continuous special inspection of adhesive anchors or post-installed reinforcing bars installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed in accordance with ACI 318-14 17.8.2.4, 26.7.1(h) and 26.13.3.2 (c) or ACI 318-11 D.9.2.4, as applicable.

Under the IBC, additional requirements as set forth in Sections 1705, 1706 or 1707 must be observed, where applicable.

4.5 Compliance with NSF/ANSI Standard 61:

The Würth WIT-UH 300 Adhesive Anchor System complies with the requirements of NSF/ANSI Standard 61, as referenced in Section 605 of the 2018, 2015, 2012, and 2009 *International Plumbing Code*® (IPC) and is certified for use as an anchoring adhesive for installing threaded rods less than or equal to 1.3 inches (33 mm) in diameter in concrete for water treatment applications.

5.0 CONDITIONS OF USE:

The Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System described in this report comply with or are a suitable alternative to what is specified in, those codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 Würth WIT-UH 300 adhesive anchors and post-installed reinforcing bars must be installed in accordance with the manufacturer's printed installation instructions included with each cartridge and provided in Figure 6 of this report.
- **5.2** The anchors and post-installed reinforcing bars described in this report must be installed in cracked and uncracked normalweight concrete having a specified compressive strength $f_c = 2,500$ psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- **5.3** The concrete shall have attained its minimum specified compressive strength, f_c , prior to installation of the anchors and post installed reinforcing bars.
- **5.4** The values of f_c used for calculation purposes must not exceed 8,000 psi (55 MPa). The value of f_c used for calculation of tension resistance must be limited to 2,500 psi (17.2 MPa) maximum for metric reinforcing bars used as anchorage in cracked concrete only.

- **5.5** Anchors and post-installed reinforcing bars must be installed in concrete base materials in holes predrilled in accordance with the instructions provided in Figure 6 of this report.
- **5.6** Loads applied to the anchors and post-installed reinforcing bars must be adjusted in accordance with Section 1605.2 of the IBC for strength design.
- 5.7 In structures assigned to Seismic Design Categories C, D, E, and F under the IBC or IRC, anchor strength must be adjusted in accordance with Section 4.1.11 of this report, and post-installed reinforcing bars must comply with Section 4.2.4 of this report.
- **5.8** Würth WIT-UH 300 adhesive anchors and post-installed reinforcing bars are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchors and post-installed reinforcing bars, subject to the conditions of this report.
- 5.9 Strength design values of the post-installed anchors are established in accordance with Section 4.1 of this report.
- **5.10** Post-installed reinforcing bar development and splice lengths are established in accordance with Section 4.2 of this report.
- **5.11** Minimum anchor spacing and edge distance as well as minimum member thickness must comply with the values described in this report.
- **5.12** Post-installed reinforcing bar spacing, minimum member thickness, and cover distance must be in accordance with the provisions of ACI 318 for cast-in place bars and Section 4.2.3 of this report.
- 5.13 Prior to installation of anchors and post-installed reinforcing bars, calculations and details demonstrating compliance with this report must be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- **5.14** Anchors and post-installed reinforcing bars are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, the anchors and post-installed reinforcing bars are permitted for installation in fire-resistive construction provided that at least one of the following conditions is fulfilled:
 - Anchors and post-installed reinforcing bars are used to resist wind or seismic forces only.
 - Anchors and post-installed reinforcing bars that support gravity load-bearing structural elements are
 within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive
 materials, or have been evaluated for resistance to fire exposure in accordance with recognized
 standards.
 - Anchors and post-installed reinforcing bars are used to support non-structural elements.
- **5.15** Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors and post-installed reinforcing bars subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- **5.16** Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.
- **5.17** Use of hot-dipped galvanized carbon steel and stainless-steel rod is permitted for exterior exposure or damp environments.
- 5.18 Steel anchoring elements in contact with preservative-treated and fire-retardant-treated wood shall be of zinc-coated steel or stainless steel. The minimum coating weights for zinc-coated steel shall be in accordance with ASTM A153.
- **5.19** Periodic special inspection must be provided in accordance with Section 4.4 in this report. Continuous special inspection for anchors and post-installed reinforcing bars installed in horizontal or upwardly inclined orientations to resist sustained tension loads must be provided in accordance with Section 4.4 of this report.
- **5.20** Installation of anchors and post-installed reinforcing bars in horizontal or upwardly inclined orientations to resist sustained tension loads must be performed by personnel certified by an applicable certification program in accordance with ACI 318-14 17.8.2.2 or 17.8.2.3 or ACI 318-11 D.9.2.2 or D.9.2.3, as applicable.
- **5.21** Würth WIT-UH 300 adhesive anchors and post-installed reinforcing bars may be used to resist tension and shear forces in floor, wall for overhead installations into concrete with a temperature between 23°F and 104°F (-5°C and 40°C) for threaded rods and rebar.

- **5.22** Anchors and post-installed reinforcing bars shall not be used for installations where the concrete temperature can vary from 40°F (5°C) or less to 80°F (27°C) or higher within a 12-hour period. Such applications may include but are not limited to anchorage of building facade systems and other applications subject to direct sun exposure.
- 5.23 Würth WIT-UH 300 adhesive is manufactured under a quality-control program with inspections by ICC-ES.

6.0 EVIDENCE SUBMITTED

Data in accordance with the ICC-ES Acceptance Criteria for Post-Installed Adhesive Anchors in Concrete (AC308), dated October 2017 (editorially revised March 2018), which incorporates requirements in ACI 355.4-11 for use in cracked and uncracked concrete; including, but not limited to, tests under freeze/thaw conditions, tests under sustained load, tests for installation including installation direction and condition, tests at elevated temperatures, tests for resistance of alkalinity, tests for resistance to sulphur and tests for seismic tension and shear.

7.0 IDENTIFICATION

- 7.1 Würth WIT-UH 300 adhesive is identified by packaging labelled with the company's name (Adolf Würth GmbH & Co. KG) and address, anchor name, the lot number, the expiration date, and the evaluation report number (ESR-4466). Threaded rods, nuts, washers, and deformed reinforcing bars must be standard steel anchor elements and must conform to applicable national or international specifications as set forth in Tables 2 and 3 of this report.
- **7.2** The report holder's contact information is the following:

ADOLF WÜRTH GmbH & Co. KG REINHOLD-WÜRTH-STRABE 12-17 74653 KÜNZELSAU GERMANY +49 (7940) 15 0 www.wuerth.de info@wuerth.de

TABLE 1—DESIGN STRENGTH - TABLE REFERENCE INDEX

DESIGN	STRENGTH ¹ - TREADED RODS	Fractional	Metric
	Steel Strength - N_{sa} , V_{sa}	Table 4	Table 10
	Concrete Strength - N_{ph} , N_{sb} , N_{sbg} , N_{cb} , N_{cbg} , V_{cb} , V_{cbg} , V_{cp} , V_{cpg}	Table 5	Table 11
3	Bond Strength ² - N _a , N _{ag}	Table 6	Table 12
DESIGN ST	RENGTH1 - REINFORCING STEEL	Fractional	Metric
	Steel Strength - N _{sa} , V _{sa}	Table 7	Table 13
<i>MATTER CONTRACTOR</i>	Concrete Strength - Npn, Nsb, Nsbg, Ncb, Ncbg, Vcb, Vcbg, Vcp, Vcpg	Table 8	Table 14
X 10	Bond Strength ² - N _a , N _{ag}	Table 9	Table 15
	Determination of development length for post-installed reinforcing bar connections	Table 16	<u>Table 17</u>

¹Ref. ACI 318-14 17.3.1.1 or 318-11 D.4.1.1, as applicable.

²See Section 4.1.4 of this evaluation report.

TABLE 2—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON CARBON AND STAINLESS-STEEL THREADED ROD MATERIALS¹

	THREADED ROD SPECIFICATION		MINIMUM SPECIFIED ULTIMATE STRENGTH, f _{uta}	MINIMUM SPECIFIED YIELD STRENGTH 0.2 PERCENT OFFSET, fya	f _{uta} /f _{ya}	ELONGATION, MIN. PERCENT ¹¹	REDUCTION OF AREA, MIN. PERCENT	SPECIFICATION FOR NUTS ¹²
	ASTM A193 ² Grade B7	psi (MPa)	125,000 (860)	105,000 (720)	1.19	16	50	ASTM A194 / A563 Grade DH
	ASTM A36 ³ / F1554 ⁴ , Grade 36	psi (MPa)	58,000 (400)	36,000 (250)	1.61	23	40	ASTM A194 / A563
	ASTM F1554 ⁴ Grade 55	psi (MPa)	75,000 (515)	55,000 (380)	1.36	23	40	Grade A
TEEL	ASTM F1554 ⁴ Grade 105	psi (MPa)	125,000 (860)	105,000 (725)	1.19	15	45	
CARBON STEEL	ASTM A449 ⁵ (³ / ₈ " to1" dia.)	psi (MPa)	120,000 (830)	92,000 (635)	1.30	14	35	ASTM A194 / A563 Grade DH
CARE	ASTM A449 ⁵ (1 ¹ / ₄ " dia.)	psi (MPa)	105,000 (720)	81,000 (560)	1.30	14	35	
	ASTM F568M ⁶ Class 5.8 (equivalent to ISO 898-1)	psi (MPa)	72,500 (500)	58,000 (400)	1.25	10	35	A563 Grade DH DIN 934 (8-A2K) ¹³
	ISO 898-1 ⁷ Class 5.8	MPa (psi)	500 (72,500)	400 (58,000)	1.25	22	-	EN ISO 4032 Grade 6
	ISO 898-1 ⁷ Class 8.8	MPa (psi)	800 (118,000)	640 (92,800)	1.25	12	52	EN ISO 4032 Grade 8
	ASTM F593 ⁸ CW1 ³ / ₈ to ⁵ / ₈ in.	psi (MPa)	100,000 (690)	65,000 (450)	1.54	20	-	ASTM F594 Alloy
STEEL	ASTM F593 ⁸ CW2 ³ / ₄ to 1 ¹ / ₄ in.	psi (MPa)	85,000 (590)	45,000 (310)	1.89	25	-	Group 1, 2 or 3
	ASTM A193/A193M ⁹ Grade B8/B8M2, Class 2B	psi (MPa)	95,000 (655)	75,000 (515)	1.27	25	40	ASTM A194/A194M
STAINLESS	ISO 3506-1 ¹⁰ A4-70 M10-M24	MPa (psi)	700 (101,500)	450 (65,250)	1.56	40	-	EN ISO 4032
14 -11	ISO 3506-1 ¹⁰ A4-50 M27-M30	MPa (psi)	500 (72,500)	210 (30,450)	2.38	40	-	EN ISO 4032

Adhesive must be used with continuously threaded carbon or stainless-steel rod (all-thread) having thread characteristics complying with ANSI B1.1 UNC Coarse Thread Series.

TABLE 3—SPECIFICATIONS AND PHYSICAL PROPERTIES OF COMMON STEEL REINFORCING BARS

REINFORCING SPECIFICATION	UNITS	MINIMUM SPECIFIED ULTIMATE STRENGTH, futa	MINIMUM SPECIFIED YIELD STRENGTH, fya
ASTM A615 ¹ , A767 ³ , A996 ⁴	psi	90,000	60,000
Grade 60	(MPa)	(620)	(414)
ASTM A706 ² , A767 ³	psi	80,000	60,000
Grade 60	(MPa)	(550)	(414)
ASTM A615 ¹ , Grade 40	psi	60,000	40,000
	(MPa)	(415)	(275)
DIN 488 ⁵ BSt 500	MPa	550	500
	(psi)	(79,750)	(72,500)

¹Standard Specification for Deformed and Plain Carbon-Steel Bars for Concrete Reinforcement.

²Standard Specification for Alloy-Steel and Stainless-steel Bolting Materials for High temperature of High Pressure service and Other Special Purpose Applications.

³Standard Specification for Carbon Structural steel.

⁴Standard Specification for Anchor Bolts, Steel 36, 55 and 105-ksi Yield Strength.

⁵Standard Specification for Hex Cap Screws, Bolts and Studs, Heat Treated, 120/105/50 ksi Minimum Tensile Strength, General Use.

^{*}Standard Specification for Hex Cap Screws, Boils and Studs, Heat Treated, 120/10/30 ksi Minimum Tensile Strength, General Use.

*Standard Specification for Carbon and Alloy Steel external Threaded Metric Fasteners.

*Mechanical properties of fasteners made of carbon steel and alloy steel - Part 1: Bolts, Screws and Studs.

*Standard Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs.

*Standard Specification for Alloy-Steel and Stainless-Steel Bolting for High Temperature or High Pressure Service and Other Special Purpose Applications.

*Mechanical properties of corrosion-resistant stainless-steel fasteners - Part 1: Bolts, Screws and Studs.

¹¹Based on 2-in. (50 mm) gauge length except for ASTM A193, which is based on a gauge length of 4d.

¹²Nuts and washers of other grades and style having specified proof load stress greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.

¹³Nuts for metric rods.

²Standard Specification for Low-Alloy Steel Deformed and Plain Bars for Concrete Reinforcement.

³Standard specification for Zinc-Coated (Galvanized) steel Bars for Concrete Reinforcement.

⁴Standard specification for Rail-Steel and Axle-steel Deformed bars for Concrete Reinforcement.

⁵Reinforcing steel, reinforcing steel bars; dimensions and masses.

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TABLE 4—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD1

DECICNI	NEODWATION	Cumbal	l luita			Nominal F	Rod Diamete	er (inch)		
DESIGN	NFORMATION	Symbol	Units	³ / ₈	1/2	5/8	³ / ₄	⁷ /8	1	1 ¹ / ₄
Threaded	rod O.D.	d	in. (mm)	0.375 (9.5)	0.500 (12.7)	0.625 (15.9)	0.750 (19.1)	0.875 (22.2)	1.000 (25.4)	1.250 (31.8)
Threaded	rod effective cross-sectional area	Ase	in.² (mm²)	0.0775 (50)	0.1419 (92)	0.2260 (146)	0.3345 (216)	0.4617 (298)	0.6057 (391)	0.9691 (625)
554,	Nominal strength as governed by steel	N _{sa}	lb (kN)	4,495 (20.0)	8,230 (36.6)	13,110 (58.3)	19,400 (86.3)	26,780 (119.1)	35,130 (156.3)	56,210 (250.0)
ASTM A36/F1554, Grade 36	strength (for a single anchor)	V _{sa}	lb (kN)	2,695 (12.0)	4,940 (22.0)	7,860 (35.0)	11,640 (51.8)	16,070 (71.4)	21,080 (93.8)	33,725 (150.0)
J A	Reduction factor for seismic shear	α _{V,seis}	-				0.60			
STI	Strength reduction factor for tension ²	φ	-				0.75			
⋖	Strength reduction factor for shear ²	ϕ	-				0.65			
4	Nominal strength as governed by steel	N _{sa}	lb (kN)	5,815 (25.9)	10,645 (47.6)	16,950 (75.5)	25,090 (111.7)	34,630 (154.1)	45,430 (202.1)	72,685 (323.1)
ASTM F1554 Grade 55	strength (for a single anchor)	V _{sa}	lb (kN)	3,490 (15.5)	6,385 (28.6)	10,170 (45.3)	15,055 (67)	20,780 (92.5)	27,260 (121.3)	43,610 (193.9)
STN	Reduction factor for seismic shear	α _{V,seis}	-				0.60			
A A	Strength reduction factor for tension ²	ϕ	-				0.75			
	Strength reduction factor for shear ²	ϕ	-				0.65			
ω 4	Nominal strength as governed by steel		lb (kN)	9,685 (43.1)	17,735 (78.9)	28,250 (125.7)	41,810 (186.0)	57,710 (256.7)	75,710 (336.8)	121,135 (538.8)
ASTM A193 Grade B7 ASTM F1554	Strength (for a single anchor)		lb (kN)	5,810 (25.9)	10,640 (47.3)	16,950 (75.4)	25,085 (111.6)	34,625 (154.0)	45,425 (202.1)	72,680 (323.3)
STA	Reduction factor for seismic shear	α <i>v,seis</i>	-				0.60			
8 0 8 G	Strength reduction factor for tension ²	φ	-	0.75						
	Strength reduction factor for shear ²	φ	-				0.65			
0	Nominal strength as governed by steel	N _{sa}	lb (kN)	9,300 (41.4)	17,030 (76.2)	27,120 (120.9)	40,140 (178.8)	55,405 (246.7)	72,685 (323.7)	101,755 (450.0)
ASTM A449	strength (for a single anchor)	V _{sa}	lb (kN)	5,580 (24.8)	10,220 (45.7)	16,270 (72.5)	24,085 (107.3)	33,240 (148)	43,610 (194.2)	61,055 (270.0)
N T S	Reduction factor for seismic shear	α _{V,seis}	-				0.60			
¥	Strength reduction factor for tension ²	φ	-				0.75			
	Strength reduction factor for shear ²	φ	-				0.65			
Σ	Nominal strength as governed by steel	N _{sa}	lb (kN)	5,620 (25)	10,290 (46)	16,385 (73)	24,250 (108)	33,470 (149)	43,910 (195.5)	70,260 (312.5)
ASTM F568M Class 5.8	strength (for a single anchor)	V _{sa}	lb (kN)	3,370 (15)	6,175 (27.6)	9,830 (43.8)	14,550 (64.8)	20,085 (89.4)	26,350 (117.3)	42,155 (187.5)
∏™	Reduction factor for seismic shear	α _{V,seis}	-				0.60			
AS	Strength reduction factor for tension ²	ϕ	-				0.65			
	Strength reduction factor for shear ²	φ	-				0.60			
×	Nominal strength as governed by steel	N _{sa}	lb (kN)	7,750 (34.5)	14,190 (63.1)	22,600 (100.5)	28,430 (126.5)	39,245 (174.6)	51,485 (229.0)	82,370 (366.4)
1 F593 CW tainless	strength (for a single anchor)	V _{sa}	lb (kN)	4,650 (20.7)	8,515 (37.9)	13,560 (60.3)	17,060 (75.9)	23,545 (104.7)	30,890 (137.4)	49,425 (219.8)
M F	Reduction factor for seismic shear	α _{V,seis}	_				0.60			
ASTM	Strength reduction factor for tension ²	φ	-				0.65			
	Strength reduction factor for shear ²	φ	-				0.60			
93M M2,	Nominal strength as governed by steel	N _{sa}	lb (kN)	7,365 (32.8)	13,480 (60.3)	21,470 (95.6)	31,780 (141.5)	43,860 (195.2)	57,540 (256.1)	92,065 (409.4)
ASTM A193/A193M Grade B8/B8M2, Class 2B	strength (for a single anchor)	V _{sa}	lb (kN)	4,420 (19.7)	8,090 (36.2)	12,880 (57.4)	19,070 (84.9)	26,320 (117.1)	34,525 (153.7)	55,240 (245.6)
I A1 de E Slas	Reduction factor for seismic shear	α _{V,seis}	-				0.60			
STN Srac	Strength reduction factor for tension ²	φ	-				0.75			
AS C	Strength reduction factor for shear ²	φ	-				0.65			

¹Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must comply with requirements for the rod.

²The tabulated value of *φ* applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI

²The tabulated value of ϕ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318-11 D.4.4.

TABLE 5—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT1

DECICAL INFORMATION	O	11:4			Nomina	al Rod Diamete	er (inch)					
DESIGN INFORMATION	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	1 ¹ / ₄			
Effectiveness factor for cracked concrete	K _{c,cr}	in-lb (SI)				17 (7)						
Effectiveness factor for uncracked concrete	K _{c,uncr}	in-lb (SI)				24 (10)						
Min. anchor spacing	Smin	in. (mm)	1 ⁷ / ₈ (48)	2 ¹ / ₂ (64)	3 (76)	3 ³ / ₄ (95)	4 ¹ / ₄ (108)	4 ³ / ₄ (121)	5 ⁷ / ₈ (149)			
Min. edge distance	Cmin	in. (mm)	1 ⁵ / ₈ (41)	1 ³ / ₄ (44)	2 (51)	2 ³ / ₈ (60)	2 ¹ / ₂ (64)	2 ³ / ₄ (70)	3 ¹ / ₄ (82)			
iii. cage distance		(111111)	,	(44)	For smaller edge distances see Section 4.1.9 of this report.							
Min. member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ + 30)			$h_{ef} + 2d_0^3$					
Critical edge distance - splitting (for uncracked concrete) ²	Cac	-			See Sec	ction 4.1.10 of th	is report.					
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-		0.65								
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-				0.70						

TABLE 6—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT1

	DESIGN INFOR	DMATION	Cumbal	Units		No	minal Ro	od Diam	eter (in	ch)	
	DESIGN INFOR	RMATION	Symbol	Units	3/8	1/2	5/8	3/4	⁷ / ₈	1	1 ¹ / ₄
Minimum embedme	ent	h _{ef,min}	in. (mm)	2 ³ / ₈ (60)	2 ³ / ₄ (70)	3 ¹ / ₈ (79)	3 ¹ / ₂ (89)	3 ¹ / ₂ (89)	4 (102)	5 (127)	
Maximum embedm	nent		h _{ef,max}	in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	25 (635)
Temperature	Tk,uncr	psi (N/mm²)	2,600 (17.9)	2,415 (16.6)	2,260 (15.6)	2,140 (14.8)	2,055 (14.2)	2,000 (13.8)	1,990 (13.7)		
range A ^{2,3} :	Characteristic bond	strength in cracked concrete	Tk,cr	psi (N/mm²)	1,040 (7.2)	1,040 (7.2)	1,110 (7.7)	1,220 (8.4)	1,210 (8.4)	1,205 (8.3)	1,145 (7.9)
Temperature	Characteristic bond	strength in uncracked concrete	Tk,uncr	psi (N/mm²)	2,265 (15.6)	2,100 (14.5)	1,970 (13.6)	1,865 (12.8)	1,785 (12.3)	1,740 (12.0)	1,730 (11.9)
range B ^{2,3} :	Characteristic bond	strength in cracked concrete	Tk,cr	psi (N/mm²)	905 (6.2)	905 (6.2)	965 (6.7)	1,060 (7.3)	1,055 (7.3)	1,050 (7.2)	995 (6.9)
Temperature	Characteristic bond	strength in uncracked concrete	Tk,uncr	psi (N/mm²)	1,630 (11.2)	1,515 (10.4)	1,420 (9.8)	1,345 (9.3)	1,290 (8.9)	1,255 (8.6)	1,250 (8.6)
range C ^{2,3} :	Characteristic bond	Tk,cr	psi (N/mm²)	650 (4.5)	655 (4.5)	695 (4.8)	765 (5.3)	760 (5.2)	755 (5.2)	720 (5.0)	
	MAC ⁴ cleaning	-	-	2	2	2	Not				
Dry	WAC* cleaning	Strength reduction factor	ϕ_{d}	-	0.55	0.55	0.55		арр	olicable	
concrete	CAC algoring	Anchor category	-	-	1	1	1	1	1	1	1
	CAC cleaning	Strength reduction factor	ϕ_{d}	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC ⁴ cleaning	Anchor category	-	-	3	2	2			Not	
Water-saturated	WACTCleaning	Strength reduction factor	φws	-	0.45	0.55	0.55		арр	olicable	
concrete	CAC cleaning	Anchor category	-	-	2	2	2	2	2	2	2
	CAC cleaning	Strength reduction factor	φws	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled holes	CAC alganiza	Anchor category	_	-	3	3	3	3	3	3	3
vvaler-illed noies	Vater-filled holes CAC cleaning Strength reduction factor			-	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction factor fo	r seismic tension		∝N,seis	-				0.95			

Bond strength values correspond to concrete compressive strength $f_c = 2,500$ psi. For concrete compressive strength, f_c between 2,500 psi and 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.10}$. See Section 4.1.4 of this report.

¹Additional setting information is described in <u>Figure 6</u>, installation instructions.

²Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of ϕ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318-11 D.4.4. $^{3}d_{0}$ = hole diameter.

²Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind, bond strengths may be increased by 23 percent for temperature range C.

⁴MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

TABLE 7—STEEL DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS 1

DECK	ON INFORMATION	Oh. al	Haita				Nominal	Bar Size				
DESIG	GN INFORMATION	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No. 10	
Reinfo	orcing bar O.D.	d	in. (mm)	0.375 (9.5)	0.500 (12.7)	0.625 (15.9)	0.750 (19.1)	0.875 (22.2)	1.000 (25.4)	1.125 (28.6)	1.250 (31.8)	
	orcing bar effective cross- nal area	A _{se}	in.² (mm²)	0.110 (71)	0.200 (129)	0.310 (200)	0.440 (284)	0.600 (387)	0.790 (510)	1.000 (645)	1.270 (819)	
"	Nominal strength as governed by steel	N _{sa}	lb (kN)	9,900 (44.0)	18,000 (80.1)	27,900 (124.1)	39,600 (176.0)	54,000 (240.0)	71,100 (316.0)	90,000 (400.0)	114,300 (508.0)	
, A996	strength (for a single anchor)	V _{sa}	lb (kN)	5,940 (26.4)	10,800 (48.0)	16,740 (74.5)	23,760 (105.7)	32,400 (144.1)	42,660 (189.8)	54,000 (240.2)	68,580 (305.0)	
ASTM A615, A767, A996 Grade 60	Reduction factor for seismic shear	αv,seis	-		0.65							
TM A6	Strength reduction factor for tension ²	φ	-				0.	65				
AS	Strength reduction factor for shear ²	φ	-		0.60							
		N _{sa}	lb	8,800	16,000	24,800	35,200	48,000	63,200	80,000	101,600	
	Nominal strength as governed by	IVsa	(kN)	(39.1)	(71.2)	(110.3)	(156.6)	(213.5)	(281.1)	(355.9)	(452.0)	
de 60	steel strength (for a single anchor)	V _{sa}	lb	5,280	9,600	14,880	21,120	28,800	37,920	48,000	60,960	
Gra		v sa	(kN)	(23.5)	(42.7)	(66.2)	(93.9)	(128.1)	(168.7)	(213.5)	(271.2)	
ASTM A706 Grade 60	Reduction for seismic shear	$a_{V,seis}$					0.	65				
AST	Strength reduction factor ϕ for tension ²	φ					0.	75				
	Strength reduction factor ϕ for shear ²	φ					0.	65				
	Nominal strength as governed by steel	N _{sa}	lb (kN)	6,600 (29.4)	12,000 (53.4)	18,600 (82.7)	26,400 (117.4)					
ade 40	strength (for a single anchor)	V _{sa}	lb (kN)	3,960 (17.6)	7,200 (32.0)	11,160 (49.6)	15,840 (70.5)		bars are furni	with ASTM A6 ished only in s		
ASTM A615 Grade 40	Reduction factor for seismic shear	α _{V,seis}	-		0.	65			throug	h No. 6		
ASTM,	Strength reduction factor for tension ²	φ	-				0.	0.65				
	Strength reduction factor for shear ²	φ	-					60				

Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable.

²The tabulated value of φ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI

^{318-14 17.3.3} or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318-11 D.4.4.

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TABLE 8—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT1

DECICN INFORMATION	Oh. a.l	Haita				Nominal	Bar Size				
DESIGN INFORMATION	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10	
Effectiveness factor for cracked concrete	K _{c,cr}	in-lb (SI)				1	7 7)				
Effectiveness factor for uncracked concrete	K _{c,uncr}	inlb. (SI)					.4 0)				
Min. anchor spacing	Smin	in. (mm)	1 ⁷ / ₈ (48)	2 ¹ / ₂ (64)	3 (76)	3 ³ / ₄ (95)	4 ¹ / ₄ (108)	4 ³ / ₄ (121)	5 ¹ / ₄ (133)	5 ⁷ / ₈ (149)	
Min. edge spacing	Cmin	in.	1 ⁵ / ₈ (41)	1 ³ / ₄	2 (51)	2 ³ / ₈ (60)	2 ¹ / ₂ (64)	2 ³ / ₄ (70)	3 (76)	3 ¹ / ₄ (82)	
		(mm)	()	(44)	For smaller edge distances see Section 4.1.9 of this report.						
Min. member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ + 30)			h _{ef} +	2d ₀ ³			
Critical edge spacing – splitting (for uncracked concrete)	C _{ac}	-			Se	e Section 4.1	.10 of this repo	ort.			
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-		0.65							
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-		0.70							

TABLE 9—BOND STRENGTH DESIGN INFORMATION FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT¹

DEGION INFOR							ı	lominal	Bar Size)		
DESIGN INFOR	DESIGN INFORMATION			Units	No.3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No.10
Minimum embed	dment	h _{ef,min}	in. (mm)	2 ³ / ₈ (60)	2 ³ / ₄ (70)	3 ¹ / ₈ (79)	3 ¹ / ₂ (89)	3 ¹ / ₂ (89)	4 (102)	4 ¹ / ₂ (114)	5 (127)	
Maximum embe	dment		h _{ef,max}	in. (mm)	7 ¹ / ₂ (191)	10 (254)	12 ¹ / ₂ (318)	15 (381)	17 ¹ / ₂ (445)	20 (508)	22 ¹ / ₂ (572)	25 (635)
Characteristic bond strength in uncracked concrete				psi (N/mm²)	2,200 (15.2)	2,100 (14.5)	2,030 (14.0)	1,970 (13.6)	1,920 (13.2)	1,880 (13.0)	1,845 (12.7)	1,815 (12.5)
range A ^{2,3} :	Characteristic be	ond strength in cracked concrete	Tk,cr	psi (N/mm²)	1,090 (7.5)	1,055 (7.3)	1,130 (7.8)	1,170 (8.1)	1,175 (8.1)	1,155 (8.0)	1,140 (7.9)	1,165 (8.0)
Temperature	Characteristic be	ond strength in uncracked concrete	Tk,uncr	psi (N/mm²)	1,915 (13.2)	1,830 (12.6)	1,765 (12.2)	1,715 (11.8)	1,670 (11.5)	1,635 (11.3)	1,615 (11.1)	1,580 (10.9)
range B ^{2,3} :	Characteristic be	ond strength in cracked concrete	Tk,cr	psi (N/mm²)	945 (6.5)	915 (6.3)	980 (6.8)	1,015 (7.0)	1,020 (7.0)	1,005 (6.9)	995 (6.8)	1,010 (7.0)
Temperature	Characteristic be	Tk,uncr	psi (N/mm²)	1,380 (9.5)	1,315 (9.1)	1,270 (8.8)	1,235 (8.5)	1,205 (8.3)	1,180 (8.1)	1,155 (8.0)	1,140 (7.8)	
range C ^{2,3} :	Characteristic be	Tk,cr	psi (N/mm²)	680 (4.7)	660 (4.6)	705 (4.9)	735 (5.1)	735 (5.1)	725 (5.0)	715 (4.9)	730 (5.0)	
	MAC ⁴ cleaning	Anchor category	-	-	2	2	2	Not				
Dry	MAC cleaning	Strength reduction factor	φ _d	-	0.55	0.55	0.55			applicable		
concrete	CAC cleaning	Anchor category	-	-	1	1	1	1	1	1	1	1
	CAC cleaning	Strength reduction factor	ϕ_d	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC⁴ cleaning	Anchor category	_	1	3	2	2			Not		
Water- saturated	WAC cleaning	Strength reduction factor	$\phi_{ m ws}$	1	0.45	0.55	0.55			applicable		
concrete	CAC cleaning	Anchor category	-	-	2	2	2	2	2	2	2	2
CAC clean		Strength reduction factor	$\phi_{ m ws}$	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	CAC cleaning	Anchor category	-	-	3	3	3	3	3	3	3	3
holes	CAC cleaning	Strength reduction factor	фwf	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction factor	r for seismic tens	ion	∝N,seis	-	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00

Bond strength values correspond to concrete compressive strength f_c = 2,500 psi. For concrete compressive strength f_c between 2,500 psi and

¹Additional setting information is described in Figure 6, installation instructions.

²Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of ϕ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318-11 D.4.4. ${}^{3}d_{0}$ = hole diameter.

^{8,000} psi, tabulated characteristic bond strength may be increased by a factor of $(f_c/2,500)^{0.10}$. See Section 4.1.4 of this report. ²Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short term loads only, such as wind and seismic, bond strengths may be increased by 23 percent for temperature range C.

⁴MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.



TABLE 10—STEEL DESIGN INFORMATION FOR METRIC THREADED ROD1

DEGL	N INCORMATION	0	Haita				Nominal Rod [Diameter (mm)		
DESIG	INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Thread	ded rod O.D.	d	mm (in.)	10 (0.39)	12 (0.47)	16 (0.63)	20 (0.79)	24 (0.94)	27 (1.06)	30 (1.18)
	ded rod effective cross- nal area	Ase	mm² (in.²)	58.0 (0.090)	84.3 (0.131)	157 (0.243)	245 (0.380)	353 (0.547)	459 (0.711)	561 (0.870)
	Nominal strength as governed by steel strength	N _{sa}	kN (lb)	29.0 (6,518)	42.2 (9,473)	78.5 (17,643)	122.5 (27,532)	176.5 (39,668)	229.5 (51,580)	280.5 (63,043)
ISO 898-1 Class 5.8	(for a single anchor)	Vsa	kN (lb)	17.4 (3,911)	25.3 (5,684)	47.1 (10,586)	73.5 (16,519)	105.9 (23,801)	137.7 (30,948)	168.3 (37,826)
8-1 CI	Reduction factor for seismic shear	$\alpha_{V,seis}$	-				0.60			
SO 89	Strength reduction factor for tension ²	φ	-				0.65			
<u> =</u>	Strength reduction factor for shear ²	φ	-				0.60			
8	Nominal strength as governed by steel strength	N _{sa}	kN (lb)	46.4 (10,428)	67.4 (15,157)	125.6 (28,229)	196 (44,051)	282.4 (63,470)	367.2 (82,528)	448.8 (100,868)
38 8.E	(for a single anchor)	V _{sa}	kN (lb)	27.8 (6,257)	40.5 (9,094)	75.4 (16,937)	117.6 (26,431)	169.4 (38,082)	220.3 (49,517)	269.3 (60,521)
ISO 898-1 Class 8.	Reduction factor for seismic shear	$\alpha_{V,seis}$	-				0.60			
SO 89	Strength reduction factor for tension ²	φ	-				0.65			
<u> =</u>	Strength reduction factor for shear ²	φ	-				0.60			
	Nominal strength as	N _{sa}	kN (lb)	40.6 (9,125)	59 (13,263)	109.9 (24,700)	171.5 (38,545)	247.1 (55,536)	229.5 (51,580)	280.5 (63,043)
-1, steel ³	governed by steel strength (for a single anchor)	Vsa	kN (lb)	24.4 (5,475)	35.4 (7,958)	65.9 (14,820)	102.9 (23,127)	148.3 (33,322)	137.7 (30,948)	168.3 (37,826)
ISO 3506-1, stainless steel ³	Reduction factor for seismic shear	$\alpha_{V,seis}$	-				0.60			
ISC A4 sta	Strength reduction factor for tension ²	φ	-				0.65			
	Strength reduction factor for shear ²	φ	-				0.60			

¹Values provided for common rod material types based on specified strengths and calculated in accordance with ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable. Nuts and washers must comply with requirements for the rod.

TABLE 11—CONCRETE BREAKOUT DESIGN INFORMATION FOR METRIC THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT¹

DEGICAL INFORMATION	0	I I mit m			Nomi	nal Rod Diamete	er (mm)		
DESIGN INFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Effectiveness factor for cracked concrete	K _{c,cr}	SI (in-lb)				7 (17)			
Effectiveness factor for uncracked concrete	K _{c,uncr}	SI (in-lb)				10 (24)			
Min. anchor spacing	Smin	mm (in.)	50 (2)	60 (2 ³ / ₈)	75 (3)	95 (3 ³ / ₄)	115 (4 ¹ / ₂)	125 (5)	140 (5 ¹ / ₂)
Min. edge distance	Cmin	mm	40 (1 ⁵ / ₈)	45 (1 ³ / ₄)	50 (2)	60 (2 ³ / ₈)	65 (2 ¹ / ₂)	75 (3)	80 (3 ¹ / ₈)
		(in.)		(174)	For s	smaller edge dist	ances, see Sect	on 4.1.9 of this	report.
Min. member thickness	h _{min}	mm (in.)		+ 30 + 1 ¹ / ₄)			h _{ef} + 2d ₀ ³		
Critical edge distance - splitting (for uncracked concrete) ²	Cac	-			See Se	ction 4.1.10 of th	is report.		
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-				0.65			
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-				0.70			

¹Additional setting information is described in Figure 6, installation instructions.

²The tabulated value of □ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of □ must be determined in accordance with ACI 318-11 D.4.4.

³A4-70 Stainless steel (M8-M24); A4-50 Stainless steel (M27-M30).

²Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of φ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11

Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318-11 D.4.4. 3 d_0 = hole diameter.

TABLE 12—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED ROD IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT¹

	DEGIGNI	NEODWATION	Completed	I I i t		N	lominal F	Rod Diam	eter (inch	1)	
	DESIGN	NFORMATION	Symbol	Units	M10	M12	M16	M20	M24	M27	M30
Minimum embe	edment		h _{ef,min}	mm (in.)	60 (2.4)	70 (2.8)	80 (3.1)	90 (3.5)	96 (3.8)	108 (4.3)	120 (4.7)
Maximum emb	edment		h _{ef,max}	mm (in.)	200 (7.9)	240 (9.4)	320 (12.6)	400 (15.7)	480 (18.9)	540 (21.3)	600 (23.6)
Temperature	Characteristic bor	nd strength in uncracked concrete	Tk, uncr	N/mm² (psi)	17.7 (2,571)	16.9 (2,453)	15.6 (2,256)	14.6 (2,112)	13.9 (2,020)	13.7 (1,985)	13.7 (1,980)
range A ^{2,3} :	Characteristic bor	nd strength in cracked concrete	Tk,cr	N/mm² (psi)	7.2 (1,039)	7.2 (1,043)	7.7 (1,110)	8.4 (1,217)	8.3 (1,209)	8.3 (1,204)	7.9 (1,149)
Temperature	Characteristic bor	nd strength in uncracked concrete	Tk, uncr	N/mm² (psi)	15.4 (2,237)	14.7 (2,134)	13.5 (1,963)	12.7 (1,837)	12.1 (1,757)	11.9 (1,727)	11.9 (1,723)
range B ^{2,3} :	Characteristic bor	nd strength in cracked concrete	Tk,cr	N/mm² (psi)	6.2 (904)	6.3 (908)	6.7 (966)	7.3 (1,058)	7.2 (1,052)	7.2 (1,047)	6.9 (999)
Temperature	Characteristic bor	nd strength in uncracked concrete	Tk, uncr	N/mm² (psi)	11.1 (1,612)	10.6 (1,538)	9.8 (1,415)	9.1 (1,324)	8.7 (1,266)	8.6 (1,245)	8.6 (1,241)
range C ^{2,3} :	Characteristic bor	nd strength in cracked concrete	Tk,cr	N/mm² (psi)	4.5 (651)	4.5 (654)	4.8 (696)	5.3 (763)	5.2 (758)	5.2 (755)	5.0 (720)
	MAC ⁴ cleaning	Anchor category	1	-	2	2	2		N	ot	
Dry	WAC cleaning	Strength reduction factor	φa	-	0.55	0.55	0.55		appli	cable	
concrete	CAC cleaning	Anchor category	-	1	1	1	1	1	1	1	1
	CAC cleaning	Strength reduction factor	фа	1	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC ⁴ cleaning	Anchor category	-	1	3	2	2			ot	
Water- saturated	WAC cleaning	Strength reduction factor	φws	1	0.45	0.55	0.55		appli	cable	
concrete	CAC cleaning	Anchor category	-	,	2	2	2	2	2	2	2
	OAC Cleaning	Strength reduction factor	φws	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	CAC cleaning	Anchor category	-	-	3	3	3	3	3	3	3
holes	CAC cleaning	Strength reduction factor	ϕ_{wf}	1	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction fact	or for seismic tens	ion	∝N,seis	-				0.95			

¹Bond strength values correspond to concrete compressive strength f_c = 2,500 psi. For concrete compressive strength, f_c between 2,500 psi and 8,000 psi, the tabulated characteristic bond strength may be increased by a factor of $(f_c/2500)^{0.10}$. See Section 4.1.4 of this report.

²Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short-term loads only such as wind, bond strengths may be increased by 23 percent for temperature range C.

⁴MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

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TABLE 13—STEEL DESIGN INFORMATION FOR METRIC REINFORCING BARS 1

DECK	ON INFORMATION	Countries and	Hada				Nominal	Bar Size			
DESIG	GN INFORMATION	Symbol	Units	Ø 10	ø 12	ø 14	ø 16	ø 20	ø 25	ø 28	ø 32
Reinfo	orcing bar O.D.	d	mm (in.)	10 (0.394)	12 (0.472)	14 (0.551)	16 (0.630)	20 (0.787)	25 (0.984)	28 (1.102)	32 (1.260)
	orcing bar effective cross- nal area	A _{se}	mm² (in.²)	78.5 (0.112)	113.1 (0.175)	153.9 (0.239)	201.1 (0.312)	314.2 (0.487)	490.9 (0.761)	615.8 (0.954)	804.2 (1.247)
	Nominal strength as governed by steel	N _{sa}	kN (lb)	43.2 (9,739)	62.2 (14,024)	84.7 (19,088)	110.6 (24,932)	172.8 (38,956)	270.0 (60,868)	338.7 (76,353)	442.3 (99,727)
200	strength (for a single anchor)	V _{sa}	kN (lb)	25.9 (5,843)	37.3 (8,414)	50.8 (11,453)	66.4 (14,959)	103.7 (23,373)	162.0 (36,521)	203.2 (45,812)	265.4 (59,836)
488 BSt	Reduction factor for seismic shear	αv,seis	-				0.	65			
DIN 48	Strength reduction factor for tension ²	φ	-				0.	65			
	Strength reduction factor for shear ²	φ	-				0.	60			

¹Values provided for common bar material types based on specified strengths and calculated in accordance with ACI 318-14 Eq. 17.4.1.2 and Eq. 17.5.1.2 b or ACI 318-11 Eq. (D-2) and Eq. (D-29), as applicable.

TABLE 14—CONCRETE BREAKOUT DESIGN INFORMATION METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT¹

DECICAL INFORMATION	O. made c.l.	Haite				Nomi	inal Bar Size			
DESIGN INFORMATION	Symbol	Units	ø 10	ø 12	ø 14	ø 16	ø 20	Ø 25	ø 28	ø 32
Effectiveness factor for cracked concrete	K _{c,cr}	SI (in-lb)					7 (17)			
Effectiveness factor for uncracked concrete	K _{c,uncr}	SI (in-lb)					10 (24)			
Min. anchor spacing	Smin	mm (in.)	50 (2)	60 (2 ³ / ₈)	70 (2 ³ / ₄)	75 (3)	95 (3³/₄)	120 (4 ⁵ / ₈)	130 (5 ¹ / ₄)	150 (5 ⁷ / ₈)
Min. edge spacing	Cmin	mm (in.)	40 (1 ⁵ / ₈)	45 (1 ³ / ₄)	50 (2)	50 (2)	60 (2 ³ / ₈)	70 (2 ³ / ₄)	75 (3)	85 (3 ¹ / ₈)
		(111.)	(-,	(174)	F	or smaller ed	dge distances, s	ee Section 4.1	.9 of this repo	ort.
Min. member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ + 30)			h _{ef} +	2d ₀ ³		
Critical edge spacing – splitting (for uncracked concrete) ²	Cac	-				See Section	4.1.10 of this re	port.		
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-					0.65			
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-					0.70			

¹Additional setting information is described in Figure 6, installation instructions.

²The tabulated value of ϕ applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, are used. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318-11 D.4.4.

²Condition A requires supplemental reinforcement, while Condition B applies where supplemental reinforcement is not provided or where pullout or pryout governs, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. The tabulated value of *ϕ* applies when the load combinations of Section 1605.2 of the IBC, ACI 318-14 5.3 or ACI 318-11 9.2, as applicable, as set forth in ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable. If the load combinations of ACI 318-11 Appendix C are used, the appropriate value of *ϕ* must be determined in accordance with ACI 318-11 D.4.4.

³*d*₀ = hole diameter.



TABLE 15—BOND STRENGTH DESIGN INFORMATION METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT¹

DEGIGN INFORM	4471011							Nominal	Bar Size)		-
DESIGN INFORM	MATION		Symbol	Units	Ø 10	Ø 12	Ø 14	Ø 16	Ø 20	Ø 25	Ø 28	Ø 32
Minimum embedr	ment		h _{ef,min}	mm (in.)	60 (2.4)	70 (2.8)	75 (3.0)	80 (3.1)	90 (3.5)	100 (3.9)	112 (4.4)	128 (5.0)
Maximum embed	lment		h _{ef,max}	mm (in.)	200 (7.9)	240 (9.4)	280 (11.0)	320 (12.6)	400 (15.7)	500 (19.7)	560 (22.0)	640 (25.2)
Temperature	Characteristic b	ond strength in uncracked concrete	Tk,uncr	N/mm² (psi)	15.1 (2,183)	14.6 (2,121)	14.0 (2,025)	14.0 (2,025)	13.5 (1,954)	13.0 (1,886)	12.8 (1,852)	12.5 (1,813)
range A ^{2,3} :	Characteristic b	ond strength in cracked concrete	Tk,cr	N/mm² (psi)	7.5 (1,082)	7.3 (1,060)	7.9 (1,144)	8.2 (1,193)	8.2 (1,188)	8.0 (1,158)	7.9 (1,144)	8.0 (1,163)
Temperature	Characteristic b	ond strength in uncracked concrete	Tk,uncr	N/mm² (psi)	13.1 (1,899)	12.7 (1,845)	12.1 (1,762)	12.1 (1,762)	11.7 (1,700)	11.3 (1,640)	11.1 (1,611)	10.9 (1,577)
range B ^{2,3} :	Characteristic b	ond strength in cracked concrete	Tk,cr	N/mm² (psi)	6.5 (942)	6.4 (922)	6.9 (996)	7.2 (1,038)	7.1 (1,034)	6.9 (1,008)	6.9 (995)	7.0 (1,012)
Temperature range C ^{2,3} :	Characteristic b	ond strength in uncracked concrete	Tk,uncr	N/mm² (psi)	9.4 (1,369)	9.2 (1,329)	8.8 (1,270)	8.8 (1,270)	8.4 (1,225)	8.2 (1,182)	8.0 (1,161)	7.8 (1,136)
range C	Characteristic b	ond strength in cracked concrete	Tk,cr	N/mm² (psi)	4.7 (678)	4.6 (665)	4.9 (718)	5.2 (748)	5.1 (745)	5.0 (726)	4.9 (717)	5.0 (729)
	MAC ⁴ cleaning	Anchor category	_	1	2	2	2	2		No		
Dry	WAC cleaning	Strength reduction factor	ϕ a	-	0.55	0.55	0.55	0.55		Applio	cable	
concrete	CAC cleaning	Anchor category	_	-	1	1	1	1	1	1	1	1
	CAC cleaning	Strength reduction factor	ϕ a	-	0.65	0.65	0.65	0.65	0.65	0.65	0.65	0.65
	MAC ⁴ cleaning	Anchor category	_	-	3	2	2	2		No		
Water-saturated	WAC cleaning	Strength reduction factor	$\phi_{ m ws}$	-	0.45	0.55	0.55	0.55		Applio	cable	
concrete	CAC cleaning	Anchor category	_	-	2	2	2	2	2	2	2	2
	OAC Cleaning	Strength reduction factor	φ _{ws}	-	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55
Water-filled	CAC cleaning	Anchor category	-	-	3	3	3	3	3	3	3	3
holes	OAC Cleaning	Strength reduction factor	ϕ_{wf}	-	0.45	0.45	0.45	0.45	0.45	0.45	0.45	0.45
Reduction factor	for seismic tensi	on	∝N,seis	-	0.95	0.95	1.00	1.00	1.00	1.00	1.00	1.00

¹Bond strength values correspond to concrete compressive strength f_c = 2,500 psi. For concrete compressive strength f_c between 2,500 psi and 8,000 psi, tabulated characteristic bond strength may not be increased. See Section 4.1.4 of this report.

o,000 psi, tabulated characteristic bond strength may not be increased. See Section 4.1.4 of this report.

Temperature range A: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C); Temperature range B: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 161°F (72°C); Temperature range C: Maximum short term temperature = 320°F (160°C), maximum long term temperature = 212°F (100°C). Short term elevated concrete temperatures are those that occur over brief intervals, e.g. as result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³Characteristic bond strengths are for sustained loads including dead and live loads. For load combinations consisting of short term loads only, such as wind and seismic, bond strengths may be increased by 23 percent for temperature range C.

⁴MAC cleaning is only permitted for installation in uncracked concrete up to an embedment depth of 10 times anchor diameter.

TABLE 16—DEVELOPMENT LENGTH FOR U.S. CUSTOMARY UNIT REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT $^{1,\,2,\,4}$

	-	Criteria Section					Bar	size			
DESIGN INFORMATION	Symbol	of Reference Standard	Units	#3	#4	#5	#6	#7	#8	#9	#10
Nominal reinforcing bar	d _b	ASTM A615/A706	in.	0.375	0.500	0.625	0.750	0.875	1.000	1.125	1.250
diameter			(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	(28.6)	(31.8)
Nominal bar area	Ab	ASTM A615/A706	in ² (mm ²)	0.11 (71.3)	0.20 (126.7)	0.31 (197.9)	0.44 (285.0)	0.60 (387.9)	0.79 (506.7)	1.00 (644.7)	1.27 (817.3)
Development length for $f_y = 60$ ksi and $f'_c = 2.500$	la	ACI 318-14 25.4.2.3 or	in.	12.0	14.4	18.0	21.6	31.5	36.0	40.5	45.0
psi (normalweight concrete) ³	3	ACI 318-11 12.2.3	(mm)	(304.8)	(365.8)	(457.2)	(548.6)	(800.1)	(914.4)	(1028.7)	(1143)
Development length for $f_y = 60$ ksi and $f_c = 4,000$	la	ACI 318-14 25.4.2.3 or	in.	12.0	12.0	14.2	17.1	24.9	28.5	32.0	35.6
psi (normalweight concrete) ³		ACI 318-11 12.2.3	(mm)	(304.8)	(304.8)	(361.4)	(433.7)	(632.5)	(722.9)	(812.8)	(904.2)

For **SI**: 1 inch \equiv 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

$${}^{4}\left(\frac{c_{b}+K_{tr}}{d_{b}}\right)=2.5$$
, $\psi_{t}=1.0$, $\psi_{e}=1.0$, $\psi_{s}=0.8$ for $d_{b}\leq \#6$, 1.0 for $d_{b}>\#6$.

TABLE 17—DEVELOPMENT LENGTH FOR EU METRIC REINFORCING BARS IN HOLES DRILLED WITH A HAMMER DRILL AND CARBIDE BIT $^{1,\,2,\,4}$

	-	Criteria Section of					Bar size			
DESIGN INFORMATION	Symbol	Reference Standard	Units	8	10	12	16	20	25	32
Nominal reinforcing			mm	8	10	12	16	20	25	32
bar diameter	d₅	BS 4449: 2005	(in.)	(0.315)	(0.394)	(0.472)	(0.630)	(0.787)	(0.984)	(1.260)
			mm ²	50.3	78.5	113.1	201.1	314.2	490.9	804.2
Nominal bar area	Αb	BS 4449: 2005	(in²)	(80.0)	(0.12)	(0.18)	(0.31)	(0.49)	(0.76)	(1.25)
Development length for $f_y = 72.5$ ksi and		ACI 318-14	mm	305	348	417	556	871	1087	1392
$f_c = 2,500 \text{ psi}$ (normalweight concrete) ³	I _d	25.4.2.3 or ACI 318-11 12.2.3	(in.)	(12.0)	(13.7)	(16.4)	(21.9)	(34.3)	(42.8)	(54.8)
Development length for $f_y = 72.5$ ksi and		ACI 318-14	mm	305	305	330	439	688	859	1100
$f_c = 4,000 \text{ psi}$ (normalweight concrete) ³	la	25.4.2.3 or ACI 318-11 12.2.3	(in.)	(12.0)	(12.0)	(13.0)	(17.3)	(27.1)	(33.8)	(43.3)

For **SI**: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi

Development lengths in SDC C through F must comply with ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21 and Section 4.2.4 of this report.

$${}^{4}\left(\frac{c_{b}+K_{tr}}{d_{b}}\right)=2.5$$
, $\psi_{t}=1.0$, $\psi_{e}=1.0$, $\psi_{s}=0.8$ for $d_{b}<20$ mm, 1.0 for $d_{b}\geq20$ mm.

¹ Development lengths valid for static, wind, and earthquake loads (SDC A and B).

² Development lengths in SDC C through F must comply with ACI 318-14 Chapter 18 or ACI 318-11 Chapter 21 and Section 4.2.4 of this report.

 $^{^3}$ f_y and \dot{f}_c used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (d) are met to permit λ > 0.75.

¹Development lengths valid for static, wind, and earthquake loads (SDC A and B).

 $^{^3}$ f_r and f_c used in this table are for example purposes only. For sand-lightweight concrete, increase development length by 33%, unless the provisions of ACI 318-14 25.4.2.4 or ACI 318-11 12.2.4 (d) are met to permit $\lambda > 0.75$.



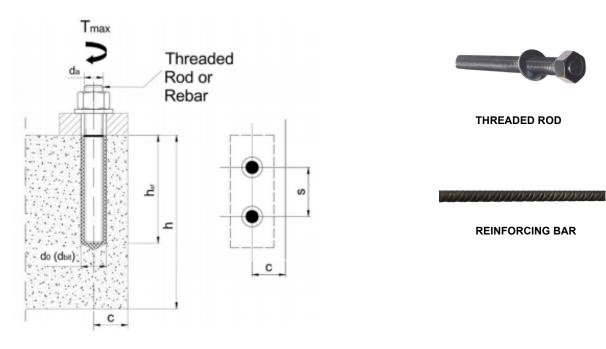


FIGURE 1—INSTALLATION PARAMETERS FOR THREADED RODS AND REINFORCING BARS



FIGURE 2—WIT-UH 300 ADHESIVE ANCHOR SYSTEM

Tool	Accessories and Shrouds	HEPA Dust Extractor
	SDS-Max and SDS-Plus Drills	
Rotary Drill Hammer	SDS-Plus and SDS-Max Hollow Drill Bit SDS-Plus and SDS-Max Drill Bit Capture Device CAT# 0903990010	Dust Extractor

FIGURE 3— WÜRTH DUST REMOVAL DRILLING SYSTEM WITH HEPA DUST EXTRACTOR OPTIONS



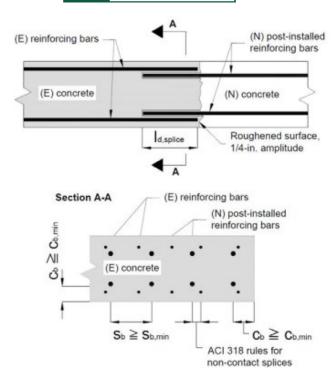


FIGURE 4—INSTALLATION PARAMETERS FOR POST-INSTALLED REINFORCING BARS

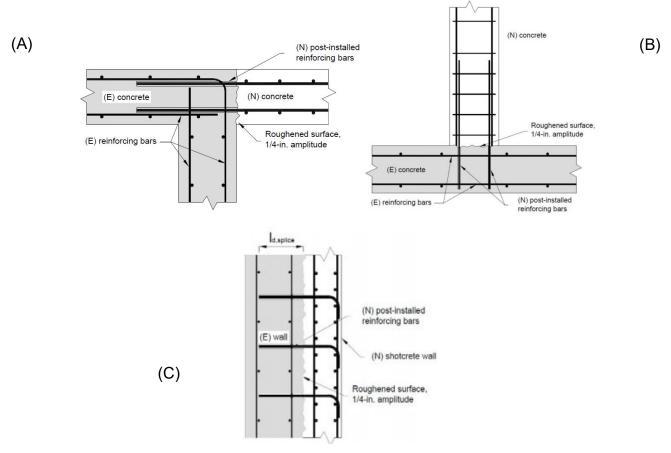


FIGURE 5—APPLICATION EXAMPLES FOR POST-INSTALLED REINFORCING BARS:
(A) TENSION LAP SPLICE WITH EXISTING FLEXURAL REINFORCEMENT; (B) TENSION DEVELOPMENT OF COLUMN DOWELS;
(C) DEVELOPMENT OF SHEAR DOWELS FOR NEWLY THICKENED SHEAR WALL

AAA

Würth WIT-UH 300 - Instruction Card

Hole cleaning Drilling Preparing CAC: Cleaning for all Cleaning for bore Ç'n 4 20. 2b. Determine brush diameter (see Table 3) for the drilled hole. Brush the hole with the 23. Starting from the bottom or back of the anchor hole, blow the hole clean compressed air (min. 6 bar / 90 psi) a minimum of two times, until return 20 2b. Determine brush diameter (see Table 3) for the drilled hole. Brush the hole Za. Starting from the bottom or back of the anchor hole, blow the hole clean with holes d₀ ≤ 3/4" (20mm) and bore hole depth h₀ ≤ 10d₄ (uncracked concrete only! hole diameter in uncracked and cracked concrete Finally blow the hole clean again with compressed air (min. 6 bar / 90 ps); a minimum of two times, until return air stream is free of noticeable dust. If the back the drilled hole is not reached an extension shall be used. When finished the hole Prior to inserting the anchor rod or rebar into the filled drilled hole, the position of the embedment depth has to be marked on the anchor. Verify anchor element is straight between 41° F - 104° F (5° C - 40° C) when in use. Review working and cure times. Consideration should be given to the reduced gel (working) time of the adhesive Check adhesive expiration date on cartridge label. Do not use expired product brush should resist insertion into the drilled hole - if not the brush is too small and must be replaced with the proper brush diameter. If the back of the drilled hole is not reached a brush extension shall be used. Finally blow the hole clean again with a handpump a minimum of four times. If the If the back of the drilled hole is not reached an extension shall be used In case of standing water in the drilled hole, all the water has to be removed from the hole (e.g. vacuum, compressed air, etc.) prior to cleaning. Precaution: Wear suitable eye and skin protection. Avoid inhalation of dusts during drilling and/or removal. (see dust extraction equipment by Würth to minimize dust dispensing adhesive into the drilled hole, separately dispense at least three full strokes of adhesive through the mixing nozzle until the adhesive is a consistent Adhesive must be properly mixed to and free of surface any way and make sure the mixing element is inside the nozzle. Load the cartridge into the correct dispensing tool. warm temperatures. For the permitted range of the base material temperature see Table 2. Attach a supplied mixing nozzle to the cartridge. Do not modify the mixer Review Safety Data Sheet (SDS) before use. Cartridge temperature must be between 41°F - 104°F (5°C - 40°C) when in use. Review working and cure tir brush is too small and must be replaced with the proper brush diameter. If the back of the drilled hole is not reached a brush extension shall be used. selected wire brush a minimum of two times (2x). A brush extension (supplied by Wurth) must be used for drill hole depth $> 6^{\circ}$ (150mm). Würth) must be used for drill hole depth > 6" (150mm). The wire brush dian is free of noticeable dust. If the back of the drilled hole is not reached an extension njection of the mixed adhesive should be clean and free of dust, must be checked periodically during use ($\emptyset_{brush} > D_{min}$, see Table 3a or 3b). The shall be used hole should be clean and free of dust, debris, ice, grease, oil or other back of the drilled hole is not reached an extension shall be used. When finished the The wire brush diameter must be checked periodically during use ($\phi_{brush} > D_{min}$ Table 3a or 3b). The brush should resist insertion into the drilled hole - if not the handpump a minimum of four times elected wire brush a minimum of two times uptions exceeding the published gel (working) time of the adhesive working and cure times into the cleaned anchor debris, ice, grease, oil or other foreign material achieve published properties new cartridges of adhesive and also for all work (2x). A brush extension (supplied by (see Table 2) prior to hole. foreign with air stream Mith

Curing and fixture

0e:00

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After full curing

of the

ightened up to

the maximum torque

(shown in , a fixture

Table 4) by using a calibrated torque can be installed to the

anchor and

Take care not to exceed the maximum torque for the selected anchor

68°F

e.g.

ю

Do not disturb,

torque or load the anchor until it is fully cured

Drill a hole into the base material with a hammer criti tool to the size and embedment required by the selected steel hardware element (see Table 4). The tolerances of the carbole drill bit must meet the requirements of ANSI Standard B212.15. Installation with piston plug. ×

Ø

1. Setting instructions for solid base material - For any application not covered by this document please contact Adolf Würth GmbH & Co. KG (ESR-4466)

of using the extension tube VL16/1,8 (Cat# 0903488122), cut the tip of the nozzle at position "X".

Piston plugs (see Table 3a or 3b) must be used with and attached to mixing and extension tube for:

with anchor rod 5/8" to 1-1/4" (M16 to M30) diameter all installations with drill hole overhead installations and installations between horizontal and overhead depth d_o >10" (250mm) and rebar sizes #5 to #10

Insert piston plug to the back of the drilled hole and inject as described in the method above. During installation the piston plug will be naturally extruded from the drilled hole by the adhesive pressure. Aftention! Do not install anchors overhead or upwardly inclined without installation hardware supplied by Würth and also receiving proper training and/or certification. (Ø14 to Ø32). Contact Würth for details prior to use.

see

7

Be sure that the anchor is fully seated at the bottom of the hole and that some adhesive has flowed from the hole and all around the top of the anchor. If there is not enough adhesive in the hole, the installation must be repeated. For overhead The anchor should be free of dirt, grease, oil or other foreign material. Push clean threaded rod or reinforcing bar into the anchor hole while turning slightly to ensure positive distribution of the adhesive until the embedment depth is reached. Observ the gel (working) time. anchor

œ

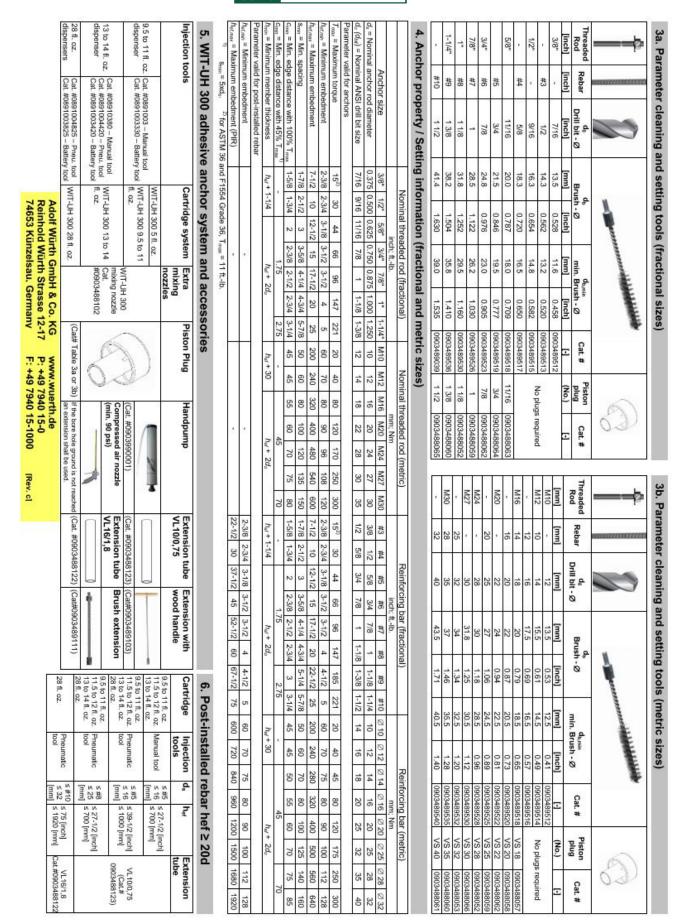
Allow the adhesive anchor to cure to the specified full curing time prior to applying any load (see Table 2). moved after place to the anchor may be performed during the gel time but the secured from moving/falling during the cure time (e.g. wedges). applications and applications between horizontal and overhead the and during cure anchor shall Minor adjustme

not be

Gel (working) times and curing times

	artridge temperature must be between 41°F (+5°C) and 104°F (+40°C)	between 41	must be	rature	e tempe	Cartrido
30 min	2 min	(+40 °C)	104 °F	to	+30 °C)	96°F (
30 min	3 min	(+29 °C)	85 °F	to	+20 °C)	:8°F (
40 min	6 min	(+19°C)	67 °F	to	+15°C)	59 °F (
1 h	10 min	(+14 °C)	58 °F	to	+10 °C)	90°F (-
2 h	15 min	(+9 °C)	49 °F	to	+5 °C)	11°F (
3.5 h	25 min	(+4 °C)	40 °F	to	(0°C)	2°F
5h	50 min	(-1 °C)	31 °F	to	(-5°C)	3°F
Full curing time	Gel (working) time	rial	emperature of base material	of ba	perature	Tem

Observe





ICC-ES Evaluation Report

ESR-4466 City of LA Supplement

Reissued October 2024

This report is subject to renewal October 2025.

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A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS

Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

ADOLF WÜRTH GmbH & CO. KG

EVALUATION SUBJECT:

WÜRTH WIT-UH 300 ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR SYSTEM IN CRACKED AND UNCRACKED CONCRETE

1.0 REPORT PURPOSE AND SCOPE

Purpose:

The purpose of this evaluation report supplement is to indicate that the Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System in cracked and uncracked concrete, described in ICC-ES evaluation report <u>ESR-4466</u>, have also been evaluated for compliance with the codes noted below as adopted by Los Angeles Department of Building and Safety (LADBS).

Applicable code editions:

- 2017 City of Los Angeles Building Code (<u>LABC</u>)
- 2017 City of Los Angeles Residential Code (<u>LARC</u>)

2.0 CONCLUSIONS

The Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System in cracked and uncracked concrete, described in Sections 2.0 through 7.0 of the evaluation report <u>ESR-4466</u>, comply with LABC Chapter 19, and LARC, and are subject to the conditions of use described in this report.

3.0 CONDITIONS OF USE

The Würth WIT-UH 300 Adhesive Anchor System and Post-Installed Reinforcing Bar System described in this evaluation report must comply with all of the following conditions:

- All applicable sections in the evaluation report <u>ESR-4466</u>.
- The design, installation, conditions of use and labeling of the anchors are in accordance with the 2015 International Building Code[®] (2015 IBC) provisions noted in the evaluation report <u>ESR-4466</u>.
- The design, installation and inspection are in accordance with additional requirements of LABC Chapters 16 and 17, as applicable.
- Under the LARC, an engineered design in accordance with LARC Section R301.1.3 must be submitted.
- The allowable and strength design values listed in the evaluation report and tables are for the connection of the anchors to
 the concrete. The connection between the anchors and the connected members shall be checked for capacity (which may
 govern).

This supplement expires concurrently with the report, reissued October 2024.





ICC-ES Evaluation Report

ESR-4466 FL Supplement

Reissued October 2024
This report is subject to renewal October 2025.

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

DIVISION: 05 00 00—METALS

Section: 05 05 19—Post-Installed Concrete Anchors

REPORT HOLDER:

ADOLF WÜRTH GmbH & CO. KG

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WÜRTH WIT-UH 300 ADHESIVE ANCHOR SYSTEM AND POST-INSTALLED REINFORCING BAR SYSTEM IN CRACKED AND UNCRACKED CONCRETE

1.0 REPORT PURPOSE AND SCOPE

Purpose:

The purpose of this evaluation report supplement is to indicate that the Würth WIT-UH 300 adhesive anchors, described in ICC-ES evaluation report ESR-4466, have also been evaluated for compliance with the codes noted below.

Applicable code editions:

- 2017 Florida Building Code—Building
- 2017 Florida Building Code—Residential

2.0 CONCLUSIONS

The Würth WIT-UH 300 adhesive anchors, described in Sections 2.0 through 7.0 of the evaluation report ESR-4466, comply with the *Florida Building Code—Building* and the *Florida Building Code—Residential*, provided the design and installation are in accordance with the 2015 *International Building Code*® provisions noted in the evaluation report.

Use of the Würth WIT-UH 300 adhesive anchors with stainless steel threaded rod materials and reinforcing bars has also been found to be in compliance with the High-Velocity Hurricane Zone provisions of the *Florida Building Code—Building* and the *Florida Building Code—Residential*.

Use of the Würth WIT-UH 300 adhesive anchors with carbon steel standard steel threaded rod materials for compliance with the High-velocity Hurricane Zone provisions of the *Florida Building Code—Building* and the *Florida Building Code—Residential* has not been evaluated and is outside the scope of the supplemental report.

For products falling under Florida Rule 9N-3, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official, when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the evaluation report, reissued October 2024.

